BOND BEHAVIOUR OF MULTI-LAYER SRG STRENGHTENING SYSTEMS TO CONCRETE

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OUTLINE

- Introduction to SRG system
- Scientific issue
- Experimental programme
- Results and discussion
- Key findings

FRPs, FRCM, and SRG Systems

INTRODUCTION

FRPs have some disadvantages:

- Low performance in fire
- Limited applicability on wet surfaces
- relatively high cost



SRG Composite System

INTRODUCTION





12345678

1 inch

Different parameters were investigated including;

- Type of substrate (masonry and concrete)
- Type of steel cords (galvanized and stainless steel cords)
- density of cords (4, 8, 12, and 23 cord/in)
- Type of matrix (lime-based, geopolymer, and fibre-reinforced)
- Bond length (100 to 400mm)

SCIENTIFIC ISSUE

Some large structural members require applying more than one layer of composite to achieve the desired capacity.

- The tensile behaviour of the strengthening composite
- The bond behaviour between the composite and the member



Test Parameters

EXPERIMENTAL PROGRAMME

- Number of steel fabric layers (1, 2, and 3 layers)
- Density of steel fabric (4 and 8 cord/in)

Density of steel fabric	Number of steel fabric layers					
	1 Layer	2 Layers	3 Layers			
4 cord/in	SB-L41	SB-L42	SB-L43			
8 cord/in	SB-L81	SB-L82	SB-L83			

Dimensions

EXPERIMENTAL PROGRAMME



Setup & Instrumentation EXPERIMENTAL PROGRAMME



EXPERIMENTAL PROGRAMME

- Concrete cubes
- Compressive strength 14 MPa

Steel fabric

Tensile strength 2800 MPa

Ultimate strain 1.5%

Mortar prisms

Compressive strength 60 MPa

Flexural strength 8 MPa

Test Results

RESULTS & DISCUSSION

• Number of layers $\propto \frac{1}{Stress in cords}$	Series	Ρ _{aν} [kN]	<i>f_{aν}</i> [MPa]	↓ [%]	s _{av} [mm]	↓ [%]
	SB-L41	20.0	2473		2.13	
	SB-L42	20.3	1257	49	1.59	25
• Number of layers $\alpha = \frac{1}{1}$	SB-L43	22.5	927	63	1.18	45
Slip of composite	SB-L81	16.7	1030		1.3	
	SB-L82	27.7	857	17	1.15	12
	SB-L83	30.6	631	39	0.92	29

Stress-Slip Curve

RESULTS & DISCUSSION

- Reduction in stress is more noticeable for higher-density fabric specimens
- Reduction in slip seems to have the same proportion for both fabrics



Three failure modes were identified, including

- rupture of the cords (1 layer of low-density fabric)
- interlaminar shear at the level of the fabric (1 layer of high-density fabric)
- substrate-composite interface debonding (2 and 3 layers of both steel fabrics)

 Failure by fabric rupture was achieved as the cords were loaded up to their ultimate strain

1 layer of 4 cord/in steel fabric



Rupture of steel cords outside the composite

Failure by interlaminar
shear was a result of high
localised stresses due to
higher cords density

1 layer of 8 cord/in steel fabric



Detachment at fabric-to-matrix interface

The use of multiple layers
can lead to a more uniform
distribution of stresses within
the composite and promote
debonding at the substrate composite interface.

2& 3 layers (both steel fabrics)



Detachment at composite-to-substrate interface

KEY FINDINGS

 Increasing the number of steel fabric layers leads to a decrease in the stress in the steel cords, as well as the slip of the composite, at failure

 Three failure modes were identified, including rupture of the cords, interlaminar shear at the level of the fabric, and substratecomposite interface debonding

Thank you



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