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### Effect of Existing Steel-to-Embedded FRP Shear Reinforcement Ratio on the Behaviour of Reinforced Concrete T-Beams

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### Background



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http://expcep.com/en/bulletin/structural-behavior-of-concrete/





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# Background

- Fibre reinforced polymers (FRPs) offer excellent mechanical and durability properties
- High strength-to-weight ratio, non-corrosive, ease of application
- But elastic brittle



### FRP SHEAR STRENGTHENING





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(a)EB unidirectional **FRP** sheets



(b)EB bi-directional FRP sheets

(c)EB laminated **FRP** sections

(d)NSM FRP reinforcement



**Deep Embedment Technique** 

- $\checkmark$  Easier to apply
- ✓ Less epoxy consumption
- ✓ Higher effectiveness





### **Research Questions**

The Effect of existing steel-to-embedded FRP shear reinforcement ratio is not quantified.
Do existing design models provide accurate predictions of the shear strength enhancement? FRP bar embedded in a drilled hole





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### Experimental programme



All dimensions in mm.



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### **Experimental programme**



All dimensions in mm.



### **Experimental programme**





Beam	Steel Shear Reinforcement Ratio	GFRP Shear Reinforcement Ratio	Steel-to-FRP Shear Reinforcement Ratio
Control	0.11%	-	-
G3	0.11%	0.125%	0.88
G6	0.11%	0.25%	0.44





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### **Experimental programme: Material Properties**

Material	Elastic modulus (GPa)	Compressive strength (MPa)	Ultimate strain mm/mm	Yield strength (MPa)	Ultimate strength (MPa)
Concrete	-	40*		-	-
Ø4mm bar			-	540	680
Ø8mm bar		-			
Ø10mm bar	200			580	680
Ø12mm bar				000	000
Ø6 mm GFRP bar	40		0.0243	-	973
* Cylindor compressive strength: Cybe strength $\sim 50.5$ MPa					

\* Cylinder compressive strength; Cube strength ≈ 50.5 MPa



## **Results: Failure Mode**



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### **Results: Failure Mode**











### **Results: Shear Force-Deflection Response**











Beam	Unstrengthened shear force capacity (kN)	Shear force at failure (kN)	Gain attributable to GFRP (kN)	Gain attributable to GFRP (%)
Control	65.5	65.5	-	-
G3	65.5	68.7	3.2	4.8
G6	65.5	90.5	25	38.1





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# Results: Strain Response (Shear Links)



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All shear links attained or exceeded the yield strain of 0.0027 Steel contribution to shear force capacity of the control beam may be computed: The yield strength (540MPa) multiplied by the cross-sectional area of the two shear links (25.1 mm<sup>2</sup> per shear link)

Vs = 27.1 kN

Vc = 65.5-27.1 = 38.4 kN



#### **Results: Strain Response (GFRP bars)**



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The FRP contribution to shear resistance ( $V_f$ ) may be calculated as the strain in the GFRP bars crossed by the shear crack that caused failure multiplied by the axial rigidity (i.e. elastic modulus multiplied by the cross-sectional area) of the GFRP bars.

Beam G6 (G2, 3,4,5 bars)

Beam G3 ( G1,2,3 bars)

Beam	V(kN)	Vs(kN)	Vf (kN)	Vc(kN)
G3	68.7	27.1	25	16.6
G6	90.5	27.1	47.8	15.6





#### **Results: Comparison between Experimental Results and TR55 Predictions**



TR55 ignores the concrete contribution to shear resistance and calculates the total shear force capacity as  $Vs + Vf = \frac{Asw}{s} * z * f_{ywd} * cot\theta + \frac{\varepsilon_{fse}E_{fd}A_f}{s_h}w_{ef}$ 



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### Summary



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- The gain in shear strength was 3.2 kN (4.8%) and 25.0 kN (38.1%) for the beams with steel-to-FRP shear reinforcement ratios of 0.88 and 0.44, respectively.
- The strengthened beams had slightly higher post-cracking stiffness than the unstrengthened control beam.
- Strain readings showed that the concrete contribution to shear resistance of the strengthened beams was about 22.5 kN (58%) less than that of the control beam.
- The FRP contribution to shear resistance decreased by 48% with the increase in steel-to-FRP shear reinforcement ratio from 0.44 to 0.88.
- TR55 design model significantly underestimated the FRP contribution to shear resistance.





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# Thank You

Any questions?

